## Chapter 8 - Examples of Designing Chrysanthemum Shells

### 8.1 Comparison of Calculated and Experimental Values

The accuracy of the empirical equation for the initial velocity of a star was examined in Section 6.5.5. The accuracy of flight velocity
can be examined by the probability deviations of the constant $n^{\prime}$ and $\log v_{o}$. Therefore, the author only compared the results obtained from the empirical equation with the results of experiment.

## Example: From the Data Given Below, Calculations of the Flight Distance of Stars.

| Calculation Number | 1 | 2 | 3 |
| :---: | :---: | :---: | :---: |
| Construction | $\mathrm{D}_{4} \mathrm{~B}_{8} \mathrm{PM}_{4}$ | $\mathrm{D}_{5} \mathrm{~B}_{12} \mathrm{HW}_{8}$ | $\mathrm{D}_{5} \mathrm{G}_{12} \mathrm{PWW}_{8}$ |
| Size of Shell | 4 sun | 5 sun | 6 sun |
| Star | $\mathrm{B}_{8}$ | $\mathrm{B}_{12}$ | $\mathrm{G}_{12}$ |
| $T_{1}$ | 0.72 s | 1.60 s | 2.92 s |
| $T_{2}$ | 0.60 s | 0.60 s | 0.60 s |
| $\delta_{1}$ | $1620 \mathrm{~kg} / \mathrm{m}^{3}$ | $1620 \mathrm{~kg} / \mathrm{m}^{3}$ | $1640 \mathrm{~kg} / \mathrm{m}^{3}$ |
| $\delta_{2}$ | $1650 \mathrm{~kg} / \mathrm{m}^{3}$ | $1650 \mathrm{~kg} / \mathrm{m}^{3}$ | $1650 \mathrm{~kg} / \mathrm{m}^{3}$ |
| $R_{1}$ | 0.00435 m | 0.00600 m | 0.00600 m |
| $R_{2}$ | 0.00250 m | 0.00250 m | 0.00250 m |
| m | 0.00055 kg | 0.00147 kg | 0.00156 kg |
| Bursting charge | P | H | P |
| A | 1.93 | 5.99 | 1.93 |
| $f$ | $7.12 \times 10^{4} \mathrm{~m}$ | $7.36 \times 10^{4} \mathrm{~m}$ | $7.12 \times 10^{4} \mathrm{~m}$ |
| $\hat{w}$ | 0.116 kg | 0.234 kg | 0.256 kg |
| Pasting paper | Kraft | Japanese paper | Japanese paper |
| a | 2.33 | 1.00 | 1.00 |
| $n$ | 4 | 8 | 8 |
| $\Delta$ | 0.30 | 0.30 | 0.30 |

Note: $\mathbf{S}$ was omitted because it is the weakest of the three and not useful except in some special cases.
(a) Calculation of Initial Velocity

Equations:
$\bar{V}=K \cdot f_{1} \cdot f_{2} \cdot f_{3}$
where
$K=5.91$
$f_{1}=(f \sigma)^{0.450}$
$f_{2}=\left(\frac{m}{\sigma}\right)^{-0.377}$
$f_{3}=A^{-0.352} e^{-\frac{13.42}{a n A}}$
(Table 7 in the Appendix)

|  | Calculation Number |  |  |
| :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 |
| $f$ | $7.12 \times 10^{4}$ | $7.36 \times 10^{4}$ | $7.12 \times 10^{4}$ |
| $\hat{w}$ | 0.116 | 0.234 | 0.256 |
| $f \hat{w}$ | $0.826 \times 10.4$ | $1.722 \times 10^{4}$ | $1.823 \times 10.4$ |
| $\mathrm{f}_{1}$ | 57.91 | 80.57 | 82.68 |
| $\sigma$ | $3.14 \times(0.00435)^{2}$ | $3.14 \times(0.00600)^{2}$ | $3.14 \times(0.00610)^{2}$ |
| m | 0.00055 | 0.00147 | 0.00156 |
| $\mathrm{m} / \sigma$ | 9.26 | 13.00 | 13.35 |
| $f_{2}$ | 0.432 | 0.380 | 0.377 |
| A | 1.93 | 5.99 | 1.93 |
| an | 9.32 | 8.00 | 8.00 |
| $f_{3}$ (Table 7 in Appendix) | 0.376 | 0.403 | 0.333 |

Multiplying $K$ by the values of $f_{1}, f_{2}$, and $f_{3}$ we have:

| Calculated $V$ | 55.6 | 72.9 | 61.3 |
| :--- | :---: | :---: | :---: |
| Experimental $V$ | 47.3 | 71.4 | 76.1 |
| Calc.V/Exp. $V$ | 1.18 | 1.02 | 0.81 |

The above table shows the coincidence of the values of initial velocity between the calculated and experimental.

## (b) Calculation of the Flight Distance of the Star in the Horizontal Direction

During the time from the start to the end of the burning of the blue or green zone, excluding the bright flash from the burst charge, the flight distance was calculated. For this process, the final velocity $v_{l}$ was first calculated.

Equations.

$$
\begin{aligned}
v_{1} & =V F_{v}\left(A_{s} b_{1}, \tau_{1}^{\prime}\right) \\
A_{s_{1}} & =0.774 V^{0.93} \frac{T_{1}^{\prime}}{R_{1} \delta_{1}} \\
b_{1} & =-\left(1-\frac{\delta_{2}}{\delta_{1}}\right)\left(\frac{R_{2}}{R_{1}}\right)^{3} \\
T_{1}^{\prime} & =\frac{T_{1}}{1-R_{2} / R_{1}} \\
\tau_{1}^{\prime} & =\frac{t_{1}}{T_{1}^{\prime}}
\end{aligned}
$$

|  | Calculation Number |  |  |
| :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 |
| $T_{1}^{\prime}$ | 1.694 | 2.744 | 5.008 |
| $R_{1}$ | 0.00435 | 0.00600 | 0.00610 |
| $\delta_{1}$ | 1620 | 1620 | 1640 |
| $V_{1} .93$ | 41.97 | 53.99 | 45.96 |
| $A_{s_{1}}$ | 7.80 | 11.79 | 17.82 |
| $b_{1}$ | 0.0034 | 0.0013 | 0.0004 |
| $\tau_{1}{ }^{\prime}$ | 0.425 | 0.583 | 0.583 |

Assuming $b=0$ and using the values of $A_{s_{1}}$ and $\tau_{1}$ ' in the table of $F_{x}$, we have:

| $F_{X}$ | 0.249 | 0.242 | 0.193 |
| :---: | :---: | :---: | :---: |
| $V^{\prime}$ | 55.6 | 72.9 | 61.3 |
| $T_{1}^{\prime}$ | 1.694 | 2.744 | 5.008 |

Multiplying the above three values mutually, we have:

| Calculated $x_{1}$ | 23.4 m | 48.5 m | 59.2 m |
| :--- | :--- | :--- | :--- |

The experimental values were:

| Experimental $x_{1}$ | 28.0 m | 52.1 m | 63.1 m |
| :---: | :---: | :---: | :---: |
| Star Number | 112 | 371 | 542 |

The value of $T_{l}$ was measured experimentally. The result shows that the calculated values of the flight distance were 3.6 to 4.6 m smaller than the experimental values.

### 8.2 An Example of Designing a Chrysanthemum Shell

In this paper only an example of designing calculations was introduced. In practical cases more important factors need to be considered: for example, ease of manufacture, efficiency of explosive, etc.

## Example: A Flower of $\mathbf{8 0} \mathbf{~ m}$ Horizontal Radius, Amber to Blue Color with a Horizontal Flight Distance of 40 m Blue and 40 m Amber.

## (a) Calculation of the Second Burning Period (Blue Colored).

From the given condition:

$$
\begin{equation*}
x_{2}=40.0=v_{1} T_{2}^{\prime} F\left(A_{s_{2}}, b_{2}, \tau_{2}^{\prime}\right) \tag{i}
\end{equation*}
$$

In this equation, $v_{l}$ is the final velocity of the star at the end of the first period and at the same time it is the initial velocity of the second period. $x_{2}$ is the distance traveled in the second period. The symbols for the first period are noted by a subscript of 1 and those of the second period are noted with a subscript 2 . Therefore:

$$
\begin{aligned}
T_{2}^{\prime} & =T_{2} \\
A_{s_{2}} & =0.774 v_{1}^{0.93} \frac{T_{2}}{R_{2} \delta_{2}}=0.774 v_{1}^{0.93} \frac{1}{w_{2} \delta_{2}}
\end{aligned}
$$

From experiment (Tables 5 and 16):

$$
\begin{aligned}
& w_{2}=0.00195 \mathrm{~m} / \mathrm{s} \\
& \delta_{2}=1620 \mathrm{~kg} / \mathrm{m}^{3}
\end{aligned}
$$

Therefore

$$
\begin{equation*}
A_{s_{2}}=0.2450 v_{1}^{0.93} \tag{ii}
\end{equation*}
$$

On the other hand the value of $v_{0.95}$ is calculated as:

$$
\begin{equation*}
v_{0.95}=v_{1} F_{v}\left(A_{s_{2}}, 0,0.95\right) \tag{iii}
\end{equation*}
$$

From (ii) several $v_{l}$ values are obtained, and from (iii) $v_{0.95}$ values are obtained as shown in the following Table.

| $A_{s_{2}}$ | $v_{1}$ | $v_{0.95}$ |
| :---: | :---: | :---: |
| 1 | 4.54 | 1.85 |
| 2 | 9.56 | 2.41 |
| 3 | 14.78 | 2.68 |
| 4 | 20.14 | 2.84 |
| 5 | 25.59 | 2.94 |
| 6 | 31.13 | 3.02 |
| 7 | 36.74 | 3.05 |
| 8 | 42.42 | 3.10 |
| 9 | 48.14 | 3.13 |
| 10 | 53.91 | 3.18 |
| 11 | 59.72 | 3.17 |
| 12 | 65.59 | 3.21 |
| 13 | 71.48 | 3.22 |
| 14 | 77.41 | 3.25 |
| 15 | 83.37 | 3.25 |
| 16 | 89.35 | 3.22 |

The relationship between the data is illustrated in Figure 46.

Figure 46 shows that when the values of $A_{s_{2}}$ exceed 9, the final velocity of the star does not increase as much. Therefore, a value of less than 9 may be desirable. The larger the value of $v_{0.95}$, the less the star is affected by gravity. For this requirement, the value of $A_{s_{2}}$ should be as large as possible under the condition $A_{s_{2}}<9$. If we use $A_{s_{2}}=9$, then we have:

$$
v_{1}=48.14, v_{0.95}=3.13
$$

Then the radius of curvature of the trajectory of the star from equation 72 is:

$$
p \cos \theta=-\frac{v^{2}}{g}=-\frac{(3.13)^{2}}{9.80}=-1.0 \mathrm{~m}
$$

The value of 1.0 m is too small. This means that the final velocity of the star is too small. However, if we possibly have stars with a large density or large final velocity, the problem may be successfully solved. From (i) we have:

$$
T_{2}=\frac{40}{v_{1} F_{x}(9,0,1)}
$$

From the above Table we have:

$$
F_{x}(9,0,1)=0.318
$$

Therefore,


Figure 46. The values that are calculated from $v_{1}$ and the function $F_{v}$.

$$
T_{2}=\frac{40}{48.14 \times 0.318}=2.61 \mathrm{~s}
$$

From this value, we can determine the radius of the second layer at the beginning of the blue:

$$
\begin{aligned}
R_{2} & =w_{2} T_{2} \\
& =0.00195 \times 2.61 \\
& =0.00509 \mathrm{~m} \\
& =5.09 \mathrm{~mm}
\end{aligned}
$$

(b) Calculation of the First Burning Period (Amber Color)

From an experiment:

$$
\begin{aligned}
\delta_{1} & =1480 \mathrm{~kg} / \mathrm{m}^{3} \\
w_{1} & =\frac{12.26-4.92}{2} / 2.17-0.60 \\
& =0.00234 \mathrm{~m} / \mathrm{s}\{4.3 .1(4) \text { or }(6)\}
\end{aligned}
$$

Connecting this period with the second period:

$$
\begin{align*}
& V F_{v}\left(A_{s_{1}}, 0, \tau_{1}^{\prime}\right)=v_{1}=48.14  \tag{iv}\\
& V T_{1}^{\prime} F_{x}\left(A_{s_{1}}, 0, \tau_{1}^{\prime}\right)=x_{1}=40 \tag{v}
\end{align*}
$$

And:

$$
\begin{aligned}
A_{s_{1}} & =0.774 V^{0.93} F \frac{1}{w_{1} \delta_{1}} \\
& =0.774 V^{0.93} \frac{1}{0.00234 \times 1480} \\
& =0.2235 V^{0.93}
\end{aligned}
$$

From this equation the relationship of $A_{s_{1}}$ and $V$ is obtained as follows:

| $A_{s_{1}}$ | 23 | 24 | 25 | 26 | 27 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $V(\mathrm{~m} / \mathrm{sec})$ | 145.6 | 152.4 | 159.3 | 166.1 | 173.1 |

In this case the final value of $\tau^{\prime}$ is unknown. It is assumed with a proper value of $\tau^{\prime}$ that the


Figure 47. The relation of $v_{1}$ and $\tau_{1}^{\prime}$.

$$
v_{1}=V F_{v}\left(A_{s_{1}}, 0, \tau_{1}^{\prime}\right)
$$

| $\tau_{1} \backslash A_{s_{1}}$ | 23 | 24 | 25 | 26 | 27 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.12 | 60.13 | 61.26 | 62.45 | 63.62 | 64.70 |
| 0.14 | 54.16 | 55.17 | 56.23 | 56.97 | 57.96 |
| 0.16 | 49.21 | 50.14 | 50.82 | 51.66 | 52.25 |
| 0.18 | 44.99 | 45.72 | 46.36 | 47.01 | 47.58 |
| 0.20 | 41.35 | 41.91 | 42.38 | 43.02 | 43.42 |
| 0.20 | 38.15 | 38.56 | 39.05 | 37.53 | 39.96 |
| 0.22 | 38.15 |  |  |  |  |

The above data are plotted as a graph in Figure 47 , and the final velocity of $v_{1}=48.14$ $\mathrm{m} / \mathrm{sec}$ is recorded as a dashed horizontal line, and the points of intersection give the value of $\tau_{1}^{\prime}$, these denote the relations of values $A_{s_{1}}$ and $\tau_{1}^{\prime}$ :


Figure 48. The relationship of $x_{1}$ and $\tau_{1}^{\prime}$.
(I)

| $A_{s_{1}}$ | 23 | 24 | 25 | 26 | 27 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\tau_{1}^{\prime}$ | 0.164 <br> 7 | 0.168 <br> 5 | 0.172 <br> 0 | 0.175 | 0.177 |
| 0 |  |  |  |  |  |

And then,

$$
\tau_{1}^{\prime}=1-R_{2} / R_{1}
$$

From this relation:

$$
R_{1}=\frac{R_{2}}{1-\tau_{1}^{\prime}}=\frac{0.00509}{1-\tau_{1}^{\prime}}
$$

On the other hand:
$T_{1}^{\prime}=\frac{T_{1}}{1-R_{2} / R_{1}}=\frac{R_{1}}{w_{1}}=\frac{R_{1}}{0.00234}=427.4 R_{1}$
Combining the above two equations:

$$
T_{1}^{\prime}=\frac{2.175}{1-\tau_{1}^{\prime}}
$$

From this, the values of $T_{1}^{\prime}$ are obtained as follows:
(I)

| $\tau_{1}^{\prime}$ | 0.12 | 0.14 | 0.16 | 0.18 | 0.20 | 0.22 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $T_{1}^{\prime}$ | 2.471 | 2.530 | 2.558 | 2.654 | 2.719 | 2.788 |

Using these values and the value of $V$, the travel distance $x_{1}$ during the first period is calculated as follows:

$$
x_{1}=V T_{1}^{\prime} F_{x}\left(A_{s}, 0, \tau_{1}^{\prime}\right)
$$

| $\tau_{1} \backslash A_{s_{2}}$ | 23 | 24 | 25 | 26 | 27 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.12 | 27.35 | 28.24 | 29.13 | 29.97 | 30.79 |
| 0.14 | 30.56 | 31.63 | 32.64 | 33.62 | 34.59 |
| 0.16 | 34.29 | 35.09 | 36.28 | 36.96 | 38.07 |
| 0.18 | 37.47 | 38.43 | 39.73 | 40.55 | 41.77 |
| 0.20 | 40.76 | 41.85 | 42.88 | 44.27 | 45.16 |
| 0.22 | 44.25 | 45.03 | 46.20 | 47.23 | 48.23 |

These values are plotted in Figure 48.
In Figure 48, the condition was given that $x$ $=40 \mathrm{~m}$. It is shown in Figure 48 as a horizontally dashed line, and when we read the value of $t_{1}^{\prime}$ at the points of intersection with the $A_{s_{2}}$ curves, we have:

(II) | $A_{s_{2}}$ | 23 | 24 | 25 | 26 | 27 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\tau_{1}^{\prime}$ | 0.195 | 0.189 | 0.182 | 0.175 | 0.170 |
| $\tau_{1}$ | 0 | 0 | 5 | 0 |  |

From the data of (I) and (II) we have the two curves on the graph in Figure 49.
The point of intersection denotes the values of $A_{s_{1}}$ and $V$ that satisfy the conditions given before:

$$
\begin{aligned}
A_{s_{2}} & =26.12 \\
\tau_{1}^{\prime} & =0.175
\end{aligned}
$$

For the value of $A_{s_{2}}$ we have:

$$
V=167.0 \mathrm{~m} / \mathrm{s}
$$

Therefore, we have:

$$
\begin{aligned}
R_{1} & =\frac{R_{2}}{1-\tau_{1}^{\prime}} \\
& =\frac{0.00509}{1-0.175} \\
& =0.00617 \mathrm{~m} \\
& =6.17 \mathrm{~mm}
\end{aligned}
$$

Therefore the diameter of the star is:

$$
\begin{aligned}
d & =0.00617 \times 2 \\
& =0.01234 \mathrm{~m} \\
& =12.3 \mathrm{~mm}
\end{aligned}
$$

Then we have:

$$
\begin{aligned}
T_{1}^{\prime} & =\frac{R_{1}-R_{2}}{w_{1}} \\
& =\frac{0.00617-0.00509}{0.00234} \\
& =0.46 \mathrm{~s}
\end{aligned}
$$

The solution to the first period is completed with the above calculations.

The burning time of the star in total:

$$
\begin{aligned}
T & =T_{1}+T_{2} \\
& =0.46+2.61 \\
& =3.07 \mathrm{~s}
\end{aligned}
$$



Figure 49. Graph for deciding the value of $A_{s_{2}}$ and $\tau_{1}^{\prime}$.

The mass of the single star:

$$
\begin{aligned}
m & =\frac{4}{3} \pi\left\{\left(R_{1}^{3}-R_{2}^{3}\right) \delta_{1}+R_{2}^{3} \delta_{2}\right\} \\
& =\frac{4}{3} \times 3.14 \times\left[\begin{array}{l}
\left\{(0.00617)^{3}-(0.00509)^{3}\right\} \\
\times 1480+(0.00509)^{3} \times 1620
\end{array}\right] \\
& =0.00153 \mathrm{~kg} \\
& =1.53 \mathrm{~g} \\
\frac{m}{\sigma} & =\frac{0.00153}{3.14 \times(0.00617)^{2}} \\
& =12.80 \mathrm{~kg} / \mathrm{m}^{2}
\end{aligned}
$$

In the above calculation it was assumed $b_{l}=0$. This is checked:

$$
\begin{aligned}
b_{1} & =-\left(1-\frac{\delta_{2}}{\delta_{1}}\right)\left(\frac{R_{2}}{R_{1}}\right)^{3} \\
& =-\left(1-\frac{1620}{1480}\right)\left(\frac{0.00509}{0.00617}\right)^{3} \\
& =0.053
\end{aligned}
$$

This value does not disturb the condition $b=0$.
The above calculation concerns the design of a star flying horizontally, but the falling height of the trajectory is as follows, ignoring air resistance:

$$
\begin{aligned}
y & =\frac{1}{2} g T^{2} \\
& =\frac{1}{2} \times 9.80 \times(3.07)^{2} \\
& =46.2 \mathrm{~m}
\end{aligned}
$$

## The Design of the Shell

First an assumption is made that there is no difference between ring star and full star shells with regard to the design conditions. As described earlier, the initial velocity of the full star is somewhat greater than that of the ring star. However, this does not affect our manufacturing process.

The initial velocity from equation 108 is:

$$
\begin{aligned}
V & =K \cdot f_{1} \cdot f_{2} \cdot f_{3} \\
& =167.0 \mathrm{~m} / \mathrm{s}
\end{aligned}
$$

From this relation we have the value of $f_{l}$ :

$$
\begin{align*}
f_{1} & =\frac{V}{K \cdot f_{2} \cdot f_{3}} \\
& =\frac{167.0}{K \cdot f_{2} \cdot f_{3}} \tag{vii}
\end{align*}
$$

On the other hand:

$$
\begin{aligned}
f_{2} & =(p / \sigma)^{-0.377} \\
& =(12.80)^{-0.377} \\
& =0.382
\end{aligned}
$$

When we use the bursting charge $\mathbf{P}$, the characteristic values are:

$$
f=7.12 \times 10^{4}, A=1.93
$$

For shell pasting, when we use Kraft paper (cement bag) for 6 layers:

$$
\begin{aligned}
a n & =2.33 \times 6 \\
& =13.98
\end{aligned}
$$

From the values of an and $A$, the values of $f_{3}$ are calculated (or from Table 7, value $f_{3}$ )

$$
\begin{aligned}
f_{3} & =A^{-0.352} e^{-\frac{13.42}{\text { anA }}} \\
& =(1.93)^{-0.352} e^{-\frac{13.42}{13.98 x . .93}} \\
& =0.483
\end{aligned}
$$

Therefore, from (vii)

$$
\begin{aligned}
f_{1} & =\frac{167.0}{5.91 \times 0.382 \times 0.483} \\
& =153.1 \\
& =(f \sigma)^{0.450}
\end{aligned}
$$

From above, the value of $f \sigma$ is

$$
f \varpi=71710 \mathrm{~kg} \cdot \mathrm{~m}
$$

When we divide $f \sigma$ by $f=71200 \mathrm{~m}$, we have 1.007 kg .

The quantity of cottonseeds $\sigma^{\prime}$, which fixes the bursting charge $\sigma$, assumes $\omega / \omega^{\prime}=16$ :

$$
\begin{aligned}
\varpi & =w / 1.600 \\
& =0.629 \mathrm{~kg} \\
\varpi^{\prime} & =0.629 \mathrm{~kg}
\end{aligned}
$$

Therefore the total mass of the burst charge is:

$$
\begin{aligned}
W & =\varpi+\varpi^{\prime} \\
& =1.007+0.629 \\
& =1.636 \\
& =1.600 \mathrm{~kg}
\end{aligned}
$$

The apparent specific gravity of the bursting charge is 0.556 and the volume of the charge is:

$$
\begin{aligned}
v & =\frac{1.636}{0.556} \\
& =2.942 \text { liters }
\end{aligned}
$$

When the volume is spherical, the radius is:

$$
\begin{aligned}
R & =\left(\frac{3}{4} \cdot \frac{1}{\pi} \times 2.942\right)^{\frac{1}{3}} \\
& =0.889 \mathrm{dm} \\
& =89 \mathrm{~mm}
\end{aligned}
$$

Including the radius of the star:

$$
R+d=101 \mathrm{~mm}
$$

Therefore the inside diameter of the shell is $d_{i}=$ $101 \times 2=202 \mathrm{~mm}$. For the 7 sun ( $\sim 8$ inch) shell, the recommended number of stars should be:

$$
\begin{aligned}
n & =4.35 \frac{D}{d}\left(\frac{D}{d}-2\right) \\
& =4.35 \times \frac{187}{12}\left(\frac{187}{12}-2\right) \\
& =922 \text { stars }
\end{aligned}
$$

The efficiency of the bursting charge when reacted should be:

$$
\begin{aligned}
r & =\frac{\text { total moving energy of stars }}{\text { energy of the burst charge }} \\
& =\frac{1}{2} \cdot m V^{2} n / \frac{f \varpi g}{\gamma-1} \\
& =\frac{1}{2} 0.00153 \times(167.0)^{2} \times 922 / \frac{71710 \times 9.80}{1.25-1} \\
& =0.0070 \\
& =0.7 \%
\end{aligned}
$$

where $\gamma$ is the adiabatic thermal expansion coefficient of the burst charge gas. The gravitational acceleration $g$ appears in the above equation because the force of explosives $f$ was calculated on the basis of a force of 1 kg -weight $\times 1$ meter, which is 9.80 joules. To convert (kg-weight $\times$ meters) into joules we must multiply by 9.80 .

